

LOW-BACKSCATTER APERTURE STRUCTURE

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DEVELOPMENT

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BACKGROUND OF THE INVENTION

Field of the Invention

The present application relates, in general, to apertures for the control and/or
measurement of light.

10 Description of the Related Art

An aperture is an opening through which light energy can pass. An aperture
can be thought of as an opening at a selected point in an optical system that determines the
size of the bundle of light rays that traverse the system. Virtually all optical systems
15 incorporate one or more apertures. For example, apertures may be used, in various optical
systems, to define a field-of-view (e.g., as used in telescopes, microscopes and other
imaging optics), define beam convergence/divergence and uniformity (e.g., as used in
collimating optics), or control the size of an image (e.g., as used in some reflectance,
transmittance, or detector response accessories).

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Within optical systems, apertures often appear in what are known in the art
as optical "trains". An optical train is typically used to control and/or measure light, and
optical systems typically have at least one, and sometimes several, optical trains. For sake
of illustration, an optical train can be treated as having three main components: a light
25 source, a controlling device (e.g., an aperture), and a detector. These components generally
are arranged in a serial manner.

With reference now to the figures, and in particular with reference now to Figure 1A, shown in side plan view is an optical train 100 consisting of a light source (e.g., a lamp) 102, an aperture (e.g., a cylinder drilled in a piece of sheet metal) 104, and a detector (e.g. a photometer) 106. Although the aperture 104, when shown in perspective view (see Figure 1B), appears circular in shape, those having ordinary skill in the art will appreciate that apertures can be quite varied in shape (e.g., circular, square, slit(s), star, or other various shapes).

Figure 1A represents the “ideal” case, in which it is assumed that the surface 108 facing the light source 102 is totally absorbing of light, and hence that the “signal strength,” or intensity, of the light detected by the detector 106 is solely indicative of the signal strength of the light source 102. When optical systems are designed analytically, it is most common for the system designers to perform the analytic calculations assuming the idealized case in their calculations. Unfortunately, actual systems rarely tend to approach the idealized case.

Referring now to Figure 2, illustrated is an optical train representative of an actual, as opposed to idealized, related-art system. As shown, in an attempt to approach the idealized case, the surface 108 facing the light source 102 is treated or prepared to be “light absorbing” (e.g., is painted black). However, also as shown, in the related art such preparations often fall short, and instead what happens is that a measurably significant amount of light 200 is reflected back from the surface 108. Depicted is that a portion of this reflected light is subsequently re-reflected such that it makes its way through the 104 aperture and is thereafter detected by the detector 106.

Those having ordinary skill in the art will recognize that the re-reflected light energy will often tend to give an indication that the light source 102 is more powerful than the light source 102 actually is (indicated in Figure 2 by making the triangles representing light energy larger than they appear in Figure 1A). Accordingly, such re-

reflected light, when considered from the standpoint of measuring the intensity or signal strength of the light source 102, is essentially "noise." Those having ordinary skill in the art will also recognize that such noise often clashes with analytical designs and calculations which assumed no, or measurably insignificant, noise. This resulting clash, at best, requires considerable subsequent work to make analytically designed systems function as desired, and, at worst, requires that the analytically designed systems be redesigned with assumptions more close to an actual system such as that depicted in Figure 2.

Consequently, it is apparent that a need exists in the art for a method and system which substantially decrease noise due to reflections from one or more surfaces below the level of that manifested in comparably sized and situated related-art systems.

BRIEF SUMMARY OF THE INVENTION

The inventors named herein ("inventors") have devised a method and system which substantially decrease optical noise below that manifested in related-art systems.

In one implementation, a system includes but is not limited to a low-backscatter aperture structure, where the system can include but is not limited to a camera, an optical communications system, an imaging system, a test system, and a measurement system.

In another implementation, a system includes but is not limited to one or more aperture-ingress-side surfaces; one or more aperture-egress-side surfaces; and the one or more aperture-ingress-side surfaces positioned such that light originating external to at least one of the one or more aperture-ingress-side surfaces is either allowed to enter an aperture ingress or is substantially reflected in a direction such that re-reflection through the aperture ingress is substantially minimized, where the system can include but is not limited to a camera, an optical communications system, an imaging system, a test system, and a measurement system.

The foregoing is a summary and thus contains, by necessity, simplifications, generalizations and omissions of detail; consequently, those skilled in the art will appreciate that the summary is illustrative only and is NOT intended to be in any way limiting. Other aspects, inventive features, and advantages of the devices and/or processes described herein, as defined solely by the claims, will become apparent in the non-limiting detailed description set forth herein

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING(S)

Figure 1A shows side plan view is an optical train 100 consisting of a light source (e.g., a lamp) 102, an aperture (e.g., a cylinder drilled in a piece of sheet metal) 104, and a detector (e.g. a photometer) 106.

Figure 1B, depicts the aperture 104 of Figure 1A in perspective view.

Figure 2, illustrates an optical train representative of an actual, as opposed to idealized, related-art system

Figure 3 shows graphically the “law” of reflection.

Figure 4A depicts what is known in the art as specular reflection.

Figure 4B illustrates what is known in the art as diffuse reflection.

Figures 5A, 5B, and 5C respectively depict in top plan, front plan, and side plan view a low-backscatter aperture structure 500 having a circular aperture 502, where the circular aperture 502 has an ingress 512 and an egress.

Figure 6 illustrates optical train 600, which is similar to optical train 100, only modified to include an implementation of the low-backscatter aperture structure 500.

Figures 7A, 7B, and 7C, respectively show in top, front, and perspective view a low-backscatter aperture structure 700 formed to be symmetrical, and having a circular aperture 702, where the circular aperture has an ingress 512 and an egress.

Figure 8 shows an optical train 800 substantially analogous to that shown in Figure 6, except that the V-shaped low-backscatter aperture structure 600 of Figure 6 has been replaced with the truncated-cone-shaped low-backscatter aperture 700 of Figure 7.

The use of the same symbols in different drawings typically indicates similar or identical items.

DETAILED DESCRIPTION OF THE INVENTION

As described above, the behaviors of related-art systems which use apertures often vary substantially from the analytic, or “ideal,” systems which have assumed “ideal” apertures for sake of simplicity in calculation and design. Also as described above, the inventors have surmised that one reason why actual systems might tend to vary substantially from ideal systems is that backscatter of light from the aperture-defining structures might be creating measurably significant noise. To further understand their beliefs with respect to the above-identified problems, following the inventors briefly examine how light can be conceptualized when simple ray tracing diagrams are used.

The inventors have surmised that backscatter can be thought of as primarily a result of light rays obeying the “law of reflection.” This law says that when a light ray is incident on a plane surface at an angle, θ , to a normal to the surface, the reflected ray also will be at that angle and in the same plane defined by the incident ray and the normal. In other words, the angle of reflection equals the angle of incidence. This law is graphically illustrated in Figure 3.

One might think that, if instead of one ray, there were multiple parallel rays striking a flat surface, the application of the law of reflection would result in the situation depicted in the Figure 4A (and in fact this is often the assumption made in many related-art optical texts and systems). However, the inventors have noticed that this type of reflection, which is typically referred as *specular* reflection within the art, generally only results when the surface is so smooth that its irregularities are small, relative to the wavelength of the incident light. The inventors have also noticed that many surfaces are not microscopically smooth and hence result in the rays in a parallel beam of light being reflected in all directions; this type of reflection, often called, *diffuse* reflection is illustrated in Figure 4B.

The inventors have surmised that when reflections such as those shown in Figures 4A and 4B result in backscatter within an optical system, measurement errors and

noise become undesirable consequences. (However, should the foregoing belief turn out not to be true, it should be noted that the subject matter herein-described still has utility, in that it has been experimentally verified to work, and hence the utility of the subject matter herein described is separate and apart from an explanation of "why" the subject matter herein described "works," or prove useful.) Accordingly, the following describes processes and devices to reduce backscatter in the direction(s) of an optical channel (e.g., the optical train 100). As will be seen, the subject matter described herein significantly reduces the need for an aperture "standoff" requirement (e.g., a requirement that the aperture 104 be a defined distance away the light source 102 so as to keep optical noise to acceptable levels), thereby providing at least the benefit of allowing optical systems to become more compact without the costs in error and noise that would be manifest in related-art systems.

In the preceding discussion of related-art aperture structures, it was surmised that the law of reflection contributes to the error and noise in optical systems. In contradistinction to the related-art, the following-described aperture structures are surmised to actually *use* the law of reflection to reduce the rays reflected along the optical train, thereby reducing the error and noise.

Referring now to Figures 5A, 5B, and 5C, respectively depicted in top plan, front plan, and side plan view is a low-backscatter aperture structure 500 having a circular aperture 502, where the circular aperture 502 has an ingress 512 and an egress (not shown). Illustrated are first and second aperture-ingress-side surfaces 504, 506, and first and second aperture-egress-side surfaces 508, 510, where the terms "ingress" and "egress" refer to the way light is preferably expected to transit the circular aperture 502. Shown is that the first and second aperture-ingress-side surfaces 504, 506 are positioned such that light originating external to at least one of the aperture-ingress-side surfaces 504, 506 is either allowed to enter the aperture ingress 512 or is substantially reflected in a direction such that re-reflection through the aperture ingress 512 is substantially minimized. Depicted is that in one embodiment this is achieved via a 45-degree angle; however, those having ordinary skill in the art will recognize that the 45-degree angle is merely an example angle, and that

many other angles can be utilized such that light originating external to at least one of the aperture-ingress-side surfaces 504, 506 is either allowed to enter the aperture ingress 512 or is substantially reflected in a direction such that re-reflection through the aperture ingress 512 is substantially minimized. For example, having at least one of the aperture-ingress-side surfaces 504, 506 placed at an acute angle relative to a plane 550 defined by an ingress 512 of the aperture 502.

Continuing to refer to Figures 5B and 5C, depicted is that in one implementation the low-backscatter aperture structure 500 is fabricated to accept a support rod 502, thereby providing a rod-mount feature sufficient to allow the low-backscatter aperture 500 to be used in optical bench setups, e.g., for test and evaluation, source measurement, etc. It has been experimentally validated that the low-backscatter aperture structure 500 produces a substantial reduction of optical noise below that observed in related-art apertures (such reduction surmised to be due to reduced backscatter). It is surmised that the V-shape of the low-backscatter aperture design changes the angle of incidence of a measurably significant portion of rays that do not pass through the aperture ingress 512. Consequently, it is further surmised that the rays are reflected at angles that direct such reflected rays away from the path of an optical system in which an implementation of the low-backscatter aperture structure 500 is utilized.

With reference now to Figure 6 illustrated is optical train 600, which is similar to optical train 100, only modified to include an implementation of the low-backscatter aperture structure 500. Shown is a surmised mechanism whereby light from the light source 102 is reflected in a direction such that re-reflection through the aperture ingress 512 is substantially minimized (e.g., such that the likely reflection of light is in a direction which would make it unlikely that light would be re-reflected through the ingress 512 of the aperture 502). For example, the reflected ray would have direction either transverse to the directional arrow 602, or have a direction whose horizontal directional component is parallel to and in the same direction as directional arrow 602. Directional

arrow 602 is intended to be representative of a line which a light ray would follow if it were to travel from ingress to egress, and directly along the axis, of aperture 502.

The foregoing pictographic illustrations of the low-backscatter aperture structure 500 described/showed the low-backscatter aperture structure 500 as having substantially flat aperture-ingress-side surfaces 504, 506. Those having ordinary skill in the art will recognize that such surfaces need not necessarily be flat, and that many different shaped surfaces can be utilized to like effect (e.g. curved surfaces can be utilized, provided such surfaces are oriented such that light originating external to the aperture-ingress-side surfaces is reflected in a direction such that re-reflection through the aperture ingress 512 is substantially minimized; that is, such that the likely reflection of light is in a direction which would make it unlikely that light would be re-reflected through the ingress 512 of the aperture 502 (e.g., the reflected ray would have direction either transverse to the directional arrow 602, or have a direction whose horizontal directional component is parallel with and in the same direction as directional arrow 602). Directional arrow 602 is intended to be representative of a line which a light ray would follow if it were to travel from ingress to egress, and directly along the axis, of aperture 502.

With respect to the aperture-ingress-side surfaces 504, 506 themselves, in some implementations at least one of the aperture-ingress-side surfaces 504, 506 is treated to substantially reflect light (e.g., is given a "mirror-like" surface, such that the likelihood of specular reflection is likely), while in other implementations at least one of the aperture-ingress-side surfaces 504, 506 is treated to substantially absorb light (e.g., is treated with black paint). In addition to the foregoing, in yet other embodiments, when a low-backscatter aperture structure 500 is to be used in an enclosed system (e.g., in a telescope), the enclosure housing the low-backscatter structure 500 is appropriately coated to enhance absorption and decrease reflections.

Referring now again to Figures 5 and 6, those skilled in the art will recognize that yet another way in which low-backscatter aperture 500 can be described is such that the one or more flat or curved surfaces are placed at an orientation whereby light

rays surmised to be obeying the law of reflection would be reflected along a path such that, absent re-reflection, the light rays would not cross plane 550 defined by the ingress 512 of the aperture 502.

5 Those having ordinary skill in the art will recognize that the low-backscatter aperture structure 500 pictographically represented in Figures 5 and 6 is geometrically constrained (i.e., asymmetrical). In another implementation, the low-backscatter structure has a substantially symmetrical structure.

10 Referring now to Figures 7A, 7B, and 7C, respectively shown in top, front, and perspective view is a low-backscatter aperture structure 700 formed to be symmetrical, and having a circular aperture 702, where the circular aperture has an ingress 712 and an egress (not shown). In contrast to the low-backscatter aperture structure 500 shown in Figures 5 and 6, in the implementation shown in Figures 7A, 7B, and 7C, the low-
15 backscatter aperture structure 700 is symmetrical. Illustrated is a first aperture-ingress-side surface 704, where the term “ingress” refers to the way light is preferably expected to transit the circular aperture 702. Shown is that the first aperture-ingress-side surface 704 is formed such that light originating external to the first aperture-ingress-side surface 704 is either allowed to enter the aperture ingress 712 or is substantially reflected in a direction
20 such that re-reflection through the aperture ingress 712 is substantially minimized. Those having ordinary skill in the art will appreciate that the sizes of low-backscatter apertures will vary depending upon application. Those skilled in the art will also recognize that the comment related to the treatment of the surface(s) (e.g., to absorb or reflect light) of the low-backscatter aperture structure 500 shown in Figure 5 apply equally well to the low-
25 backscatter aperture structure 700 shown in Figure 7.

 With reference now to Figure 8, shown is an optical train 800 substantially analogous to that shown in Figure 6, except that the V-shaped low-backscatter aperture
30 structure 500 of Figure 6 has been replaced with the truncated-cone-shaped low-backscatter

aperture 700 of Figure 7. Also shown is a surmised operation for the implementation shown, which is substantially similar to operation shown for the V-shaped implementation in Figure 6, except that the rays are surmised to have been reflected in a 360-degree pattern due to the truncated-cone shape of the low-backscatter aperture structure 700.

5 Referring now again to Figures 7 and 8, with respect to the aperture-ingress-side surface 704 itself, in some implementations the aperture-ingress-side surface 704 is treated to substantially reflect light (e.g., is given a “mirror-like” surface, such that the likelihood of specular reflection is likely), while in other implementations the aperture-ingress-side surface 704 is treated to substantially absorb light (e.g., is treated with black paint). In addition to the foregoing, in yet other embodiments, when a low-backscatter aperture structure 700 is to be used in an enclosed system (e.g., in a microscope), the enclosure housing the low-backscatter structure 700 is appropriately coated to enhance absorption and decrease reflections.

15 The inventors have hypothesized that for miniature optical systems, fixed apertures (e.g., those having specific shaped and sized aperture openings), would be the standard implementation. However, the inventors have also surmised that optical bench applications using low-backscatter aperture structures could be made more cost effective if the low-backscatter aperture structures were fabricated in such as way as to provide replaceable openings.

Referring now to Figures 9A and 9B, shown is a low-backscatter aperture structure fabricated such that it provides replaceable openings. Depicted is universal base 900 fabricated to accept interchangeable low-backscatter aperture structures 902, 904. Interchangeable low-backscatter aperture structures 902, 904 are respectively illustrated in Figure 9A, where interchangeable low-backscatter aperture structure 902 is shown with a circular opening and where interchangeable low-backscatter aperture structure 904 is shown with a slit opening. However, while only slit and circular openings are shown, openings of various sizes and shapes are contemplated. In addition, while any number of

methods of interchangeability are possible, an implementation which uses pressure spring clips is depicted in Figure 9A.

5 With reference now to Figure 9B, shown is a top-plan cutaway view depicting how interchangeable low-backscatter aperture structures 900, 902 interface with universal base 900 and are held in place by pressure clips.

10 The inventors have experimentally verified that the V-shaped low-backscatter aperture structure 500 provides lower optical noise than that arising from related-art apertures. This verification was achieved via a Gamma Scientific RS-12 regulated tungsten reference lamp, a Photo Research 1980A photometer, a 3-meter optical bench rail, mounting hardware, a related-art flat aperture with a 1-1/2-inch circular opening, and a custom-fabricated, V-shaped low-backscatter aperture structure 500, also with a 1-1/2-inch circular opening.

15 During experimental verification the reference lamp, the aperture under test, and the photometer were mounted on the optical bench rail. The photometer was focused on the front surface of the lamp. The distance between the photometer and the lamp was fixed at 136 centimeters (cm). The initial reading of the lamp was taken in a dark room without an aperture present and measured to be 348.1 foot lamberts (FL). After the initial recording, the conventional flat aperture was placed in the optical train and initially placed 20 1 cm from the front of the lamp. A reading of the light source was made at this position and at subsequent positions in 0.5-cm increments out to a distance of 20 cm from the light source. The conventional flat aperture then was replaced with a V low-backscatter aperture, and lamps measurements were repeated at the same positions.

25 The data from these measurements are plotted in Figure 10. Differences in the lamp readings can be noted for the two aperture designs for aperture positions out to approximately 9-10 cm. These differences also validate the low-backscatter concept design. While this rudimentary validation produced a relatively small, 1.27 percent,

reduction in the lamp measurement error in this macro application, this error difference was as large as 4.5 FL.

Another observation is that the fabricated example of the low-backscatter aperture tested did not *completely* eliminate the backscatter. While this residual effect was expected (hence the “low-backscatter” nomenclature), those having ordinary skill in the art will appreciate that the residual effect could be reduced further with a better “black” absorbing matte coating on the aperture and a more finely honed ridge on the front of the “V” edge of the aperture.

While the foregoing discussion has described an optical train having an implementation of the low-backscatter aperture structure, those having ordinary skill in the art will recognize that the low-backscatter aperture structure can be employed in other systems such as cameras, telescopes, microscopes or other imaging systems, an optical communications systems, and test and measurement systems (e.g., light benches). In short, virtually any system which controls and channels light can employ the low-backscatter aperture structure described herein.

The foregoing described embodiments depict different components contained within, or connected with, different other components. It is to be understood that such depicted architectures are merely exemplary, and that in fact many other architectures can be implemented which achieve the same functionality. In a conceptual sense, any arrangement of components to achieve the same functionality is effectively "associated" such that the desired functionality is achieved. Hence, any two components herein combined to achieve a particular functionality can be seen as "associated with" each other such that the desired functionality is achieved, irrespective of architectures or intermedial components. Likewise, any two components so associated can also be viewed as being "operably connected", or "operably coupled", to each other to achieve the desired functionality.

